

Heat Release Uncertainty in the NIST Large Fire Laboratory

NIST/BFRL: Advanced Measurements and
Predictive Methods Program

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In Memory



Jack Lee (1953-2007)

Large Fire Research Laboratory

- Fire Test Area (high-bay) 37 m x 9.2 m x 11 m
- Flue Gas Cleaning System – Pollution Control (2000)
- 3 Operational Fire Calorimeters
 - 9 m x 12 m hood = 10 MW Calorimeter (2003)
 - 6 m x 6 m hood = 3 MW Calorimeter (2001) NISTIR 7052
 - 3 m x 3 m hood = 500 kW Calorimeter (2005, 2007)



Examples: LFL Heat Release Rate Measurement



Underventilated
Compartment fires
for FDS validation
(*R. Johnsson*)



Wildland-Urban Interface Fires
(*W. Mell*)



Hose Stream Effectiveness (*D. Stroup*)

Heat Release Rate Measurement Method

Oxygen Consumption Principle:

$$HRR = (\Delta H_C)_{Mass_O2} (\dot{m}_{O2}^o - \dot{m}_{O2})$$

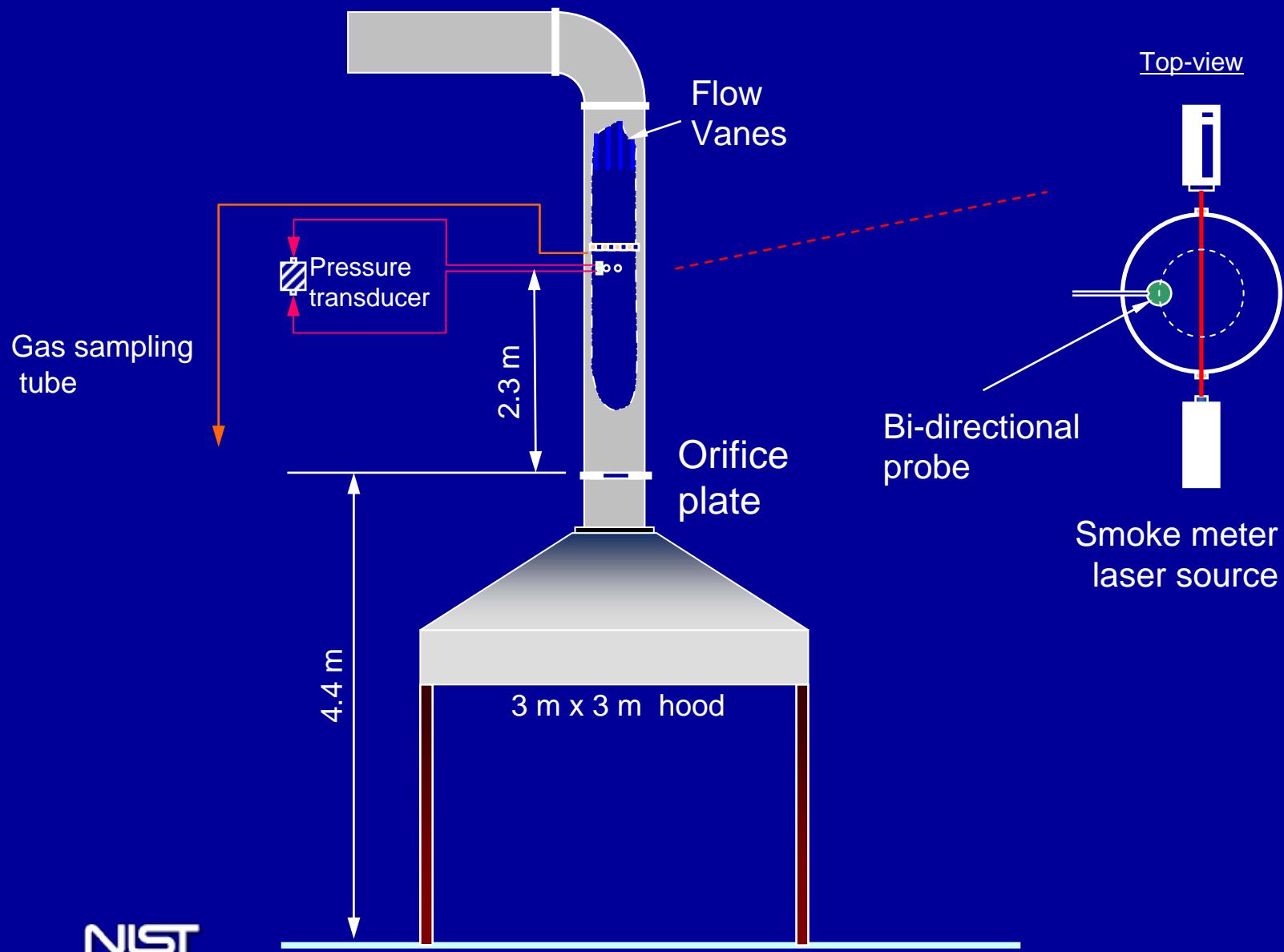
Simplifying Assumptions and Physical Measurements:

$$\frac{\dot{m}_e}{M_e} = \frac{\dot{m}_{air}}{M_{air}}(1 - \phi) + \frac{\dot{m}_{air}}{M_{air}}\phi\alpha \quad \alpha = 1 + X_{O2}^o(\beta - 1)$$

$$\phi = \frac{\dot{m}_{O2}^o - \dot{m}_{O2}}{\dot{m}_{O2}^o} = \frac{X_{O2}^o(1 - X_{CO2} - X_{CO}) - X_{O2}(1 - X_{CO2}^o)}{(1 - X_{O2} - X_{CO2} - X_{CO})X_{O2}^o}$$

$$HRR = (\Delta H_C)_{Mass_O2} \phi \frac{\dot{m}_e}{1 + \phi(\alpha - 1)} (1 - X_{H2O}^o) X_{O2}^o \frac{MW_{O2}}{MW_{air}}$$

500 kW Calorimeter Exhaust Measurements (2005)



Uncertainty Analysis

Propagation of Uncertainty:
$$U_{HRR} = k \sqrt{\left(\sum_{i=1}^n ux_i^2 \left(\frac{\partial HRR}{\partial x_i} \right)^2 \right)}$$

x_i = independent variables

ux_i = combined uncertainty of x_i , Type A and B

n = 36 (constants and measured quantities)

k = 2 (95 % confidence level)

Pros:

- Verification of HRR measurement (instead of calibration)
- Prioritize improvements to HRR measurement
- Study general trends and limiting conditions

Cons:

- Correlated variables can lead to over-estimate of uncertainty
- Unidentified physics or measurement processes can produce misleading results

Components of HRR Uncertainty

Table 1. Example of contribution of constant parameters to combined uncertainty in HRR measurement. 500 kW Calorimeter (2005), 180 kW fire.

Variable (x_i)	Units	Value	ux_i (type B)	$2 u_c x_i \frac{\partial HRR}{\partial x_i}$ (kW)	Relative Unceratinty
Energy of fuel per O2 (Ef)	kJ/kg O2	13100	350	10.37	5.3%
Energy of CO per O2 (Eco)	kJ/kg CO	17690	10	0.00	0.0%
Expansion Parameter, Alpha (α)	none	1.1	0.048	0.55	0.3%
Molecular Weight dry Air (Mair)	g/mol	28.97	0.1	1.34	0.7%
Molecular Weight Exhaust gas (Me)	g/mol	28.97	0.3	2.01	1.0%
Velocity Shape Factor=Ve/V (Kt)	none	0.85	0.025	11.42	5.9%
Velocity Probe Constant (Kp)	none	1.08	0.05	17.97	9.3%
Ideal Gas Constant (R)	m ³ Pa/K/kmol	8314.47	5.00E-03	0.00	0.0%
Duct Diameter (D)	m	0.4825	2.00E-03	3.22	1.7%
Oxygen Span Gas (O2span)	none	0.2095	5.00E-04	1.16	0.6%
Oxygen Zero Gas (O2zero)	none	0	2.00E-04	0.47	0.2%
CO ₂ Span Gas (CO2span)	none	0.02797	2.80E-04	0.51	0.3%
CO ₂ Zero Gas (CO2zero)	none	0	2.00E-05	0.51	0.3%
CO Span Gas (COspan)	none	0.0028	2.80E-05	0.00	0.0%
CO Zero Gas (COzero)	none	0	1.00E-06	0.00	0.0%
Velocity Pressure Sensitivity (Pcal)	Pa/V	133.36	5.00E-03	0.01	0.0%

Components of HRR Uncertainty

Table 2. Example of contribution of variable parameters to combined uncertainty in HRR measurement. 500 kW calorimeter (2005), 180 kW fire.

Variable (x_i)	Units	Value	ux_i (type A)	ux_i (type B)	$2 u_c x_i \frac{\partial HRR}{\partial x_i}$ (kW)	Relative Unceratinty
Oxygen Zero Voltage (O2zeroV)	V	-3.1E-03	5.0E-05	2.5E-05	0.03	0.0%
Oxygen Span Voltage (O2spanV)	V	8.4E-01	5.0E-05	2.5E-05	0.03	0.0%
Oxygen Voltage (O2V)	V	8.2E-01	2.2E-04	2.5E-05	4.28	2.2%
Ambient Oxygen (O2oV)	V	8.4E-01	2.9E-05	2.5E-05	0.75	0.4%
Oxygen Pressure Voltage (O2PCV)	V	7.4E+00	1.7E-04	2.5E-05	0.01	0.0%
Press Ref Voltage (O2PCVo)	V	7.4E+00	1.7E-04	2.5E-05	0.01	0.0%
CO ₂ Zero Voltage (CO2zeroV)	V	-3.6E-04	5.0E-04	2.5E-05	0.01	0.0%
CO ₂ Span Voltage(CO2spanV)	V	4.6E+00	5.0E-04	2.5E-05	0.01	0.0%
Carbon Dioxide Voltage (CO2V)	V	6.0E-01	3.6E-03	2.5E-05	0.35	0.2%
Ambient CO ₂ (CO2oV)	V	6.9E-02	5.5E-04	2.5E-05	0.05	0.0%
CO Span Voltage (COzeroV)	V	3.7E-04	1.0E-03	2.5E-05	0.02	0.0%
CO Zero Voltage (COspanV)	V	4.6E+00	1.0E-03	2.5E-05	0.00	0.0%
Carbon Monoxide Voltage (COV)	V	1.8E-03	5.6E-04	2.5E-05	0.01	0.0%
Exhaust Flow Pressure Voltage (PV)	V	8.8E-01	7.2E-02	2.5E-05	15.71	8.1%
Exhaust Flow Zero Voltage (PzeroV)	V	-2.7E-03	5.0E-05	2.5E-05	0.01	0.0%
Exhaust Temperature (Te)	K	3.7E+02	8.7E-01	1.3E+00	0.81	0.4%
Ambient Pressure (Pamb)	Pa	1.0E+05	2.2E+00	6.7E+02	1.30	0.7%
Ambient Relative Humidity (RH)	%	6.3E-01	4.2E-03	2.0E-02	0.00	0.0%
Ambient Temperature (Tamb)	C	2.7E+01	1.4E-02	1.3E+00	0.00	0.0%

Natural Gas Burner HRR Uncertainty

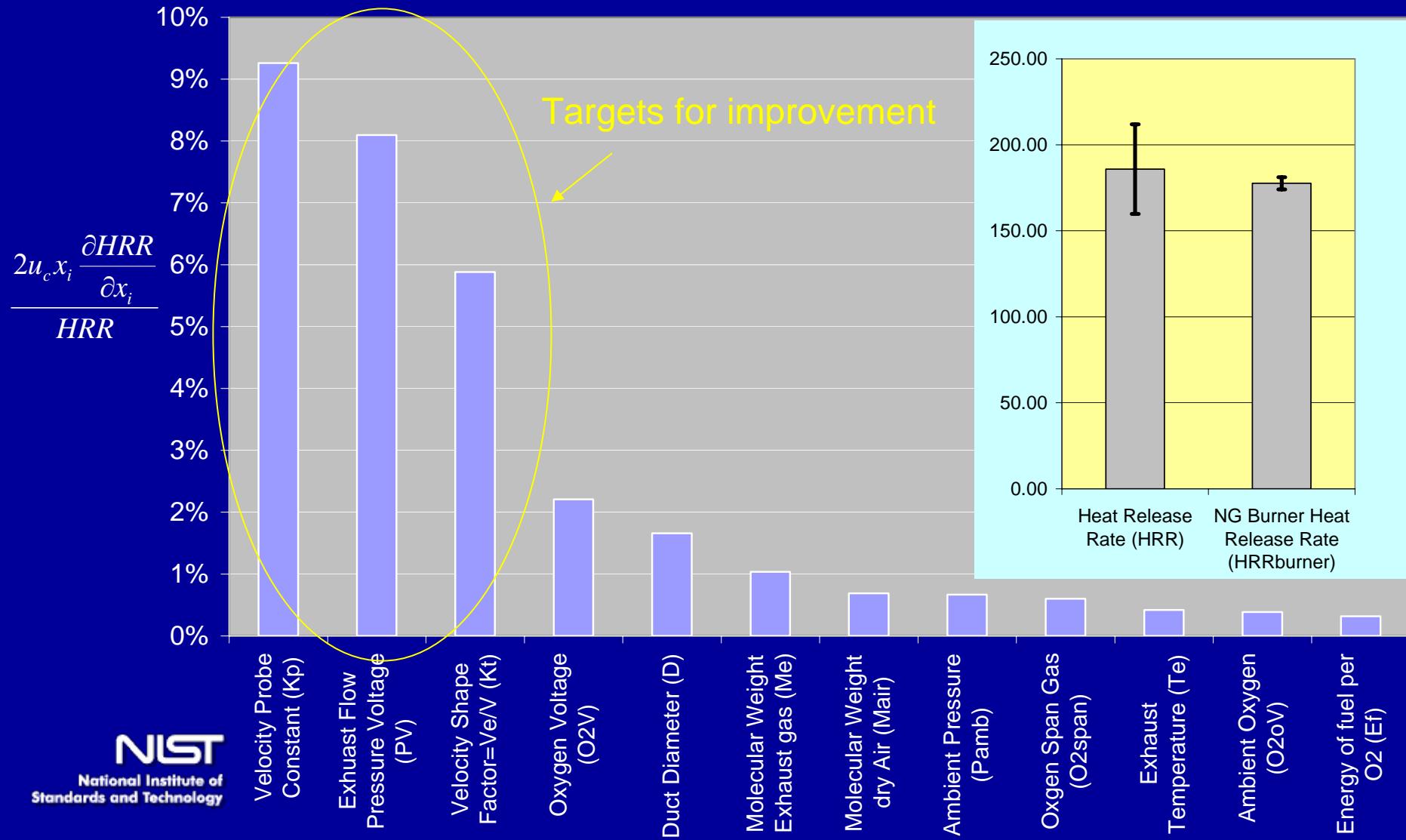
Table 3. Example of components of uncertainty in controlled natural gas fire.

Variable (x_i)	Units	Value	ux_i (type A)	ux_i (type B)	$2u_c x_i \frac{\partial HRRburner}{\partial x_i}$ (kW)	Relative Unceratinty
Natural Gas Energy Value (NGhoc)	MJ/m ³	34.027	1.0E-02	2.55E-01	2.66E+00	1.500%
NG Flowmeter Factor (K)	pulses/cm ³	0.0005	0.0E+00	3.00E-06	2.10E+00	1.181%
Pulse Counter Voltage	V	0.0857	8.3E-05	2.50E-05	3.58E-01	0.202%
Pulse Counter Zero Voltage	V	-0.0007	3.7E-05	2.50E-05	1.85E-01	0.104%
NG Pressure Voltage	V	0.0170	9.4E-07	2.50E-05	5.24E-01	0.295%
NG Pressure Gauge Sensitivity	psia/V	1658.5	0.0E+00	1.50E+00	3.21E-01	0.181%
NG Temperature	K	300.8	1.2E-02	6.40E-01	7.56E-01	0.426%
NG Burner Heat Release Rate (HRRburner)	kW	177.63			3.55	2.00%

Example: Uncertainty Results – Verification

180 kW steady natural gas fire, 3 m x 3 m hood, 2 kg/s (2005 config.)

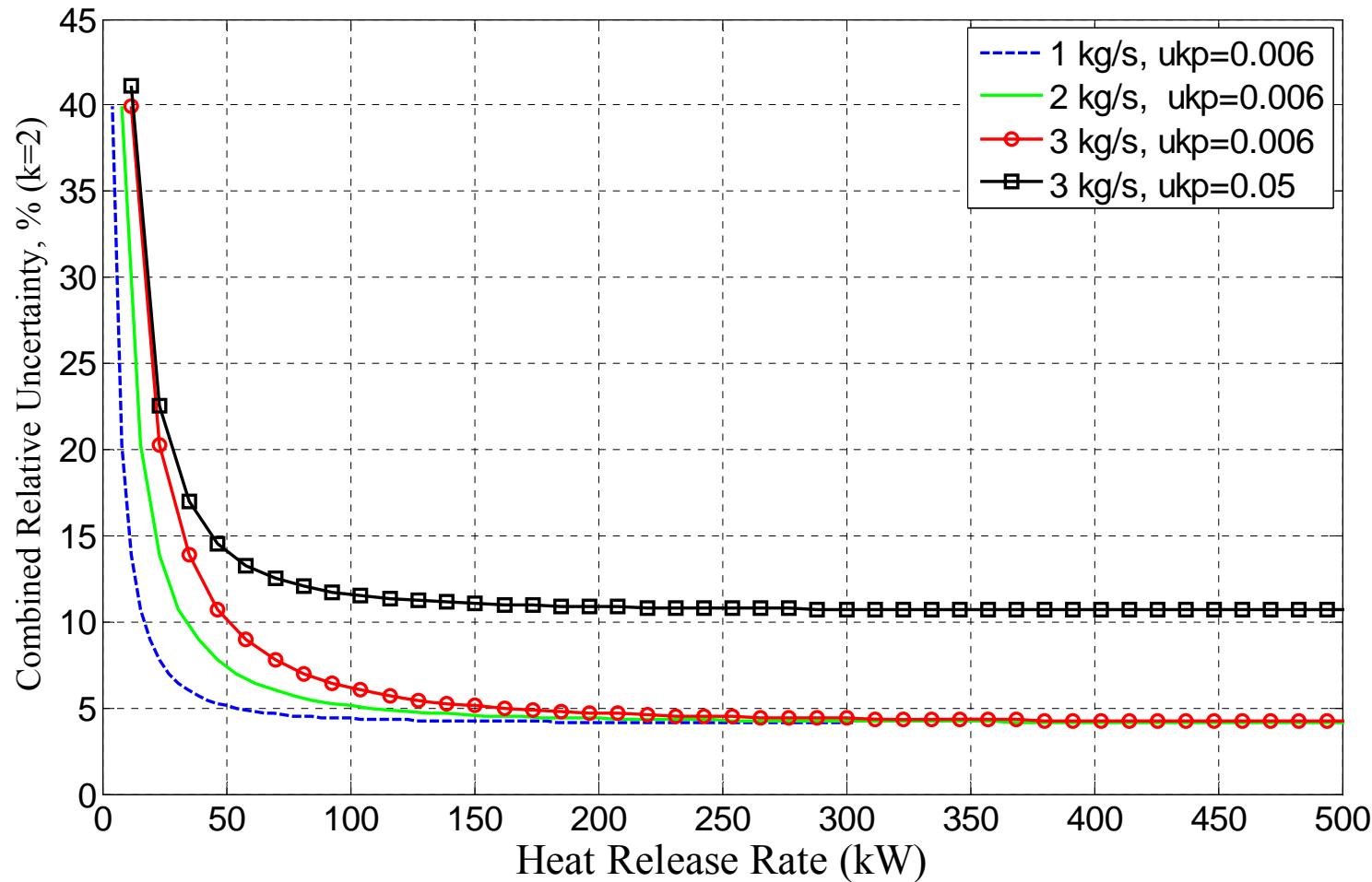
$U_{HRR} = 14\%$ (known fuel), $U_{HRR} = 15\%$ (unknown fuel),
 $U_{HRR} = 20\%$ (unknown fuel and variable fire position)



Parametric Study of HRR Uncertainty , 500 kW Calorimeter

Assume only Type B uncertainties (ideal case), Methane Fire

Observe effects of probe constant and exhaust flow rate on U_{HRR}



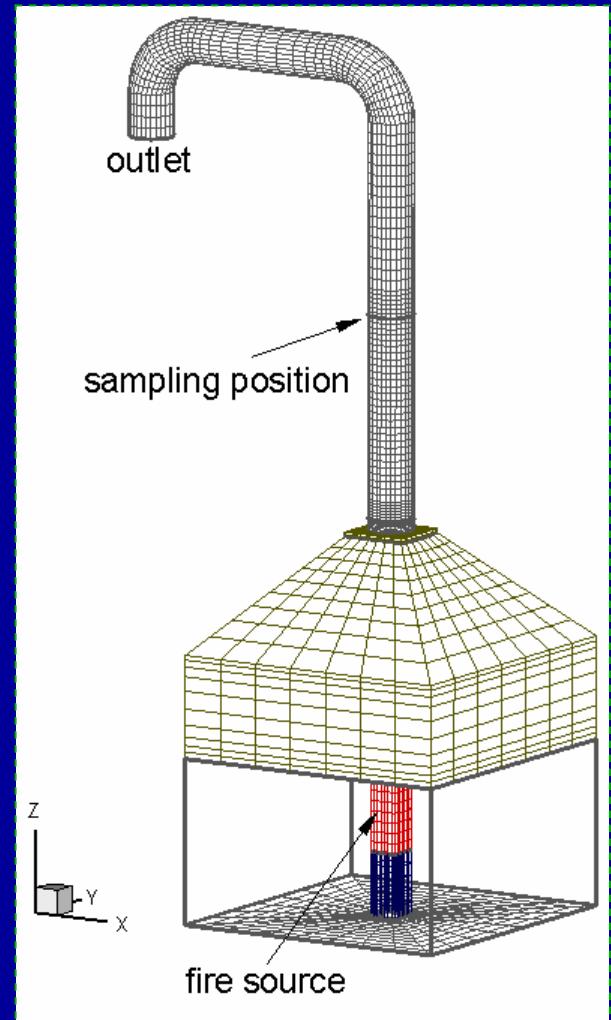
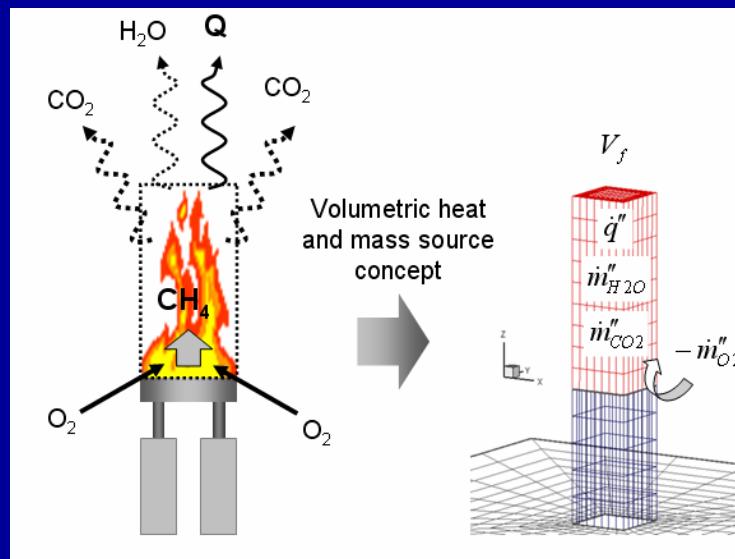
CFD model of HRR measurement

CFD Solver : FLUENT v.6.0

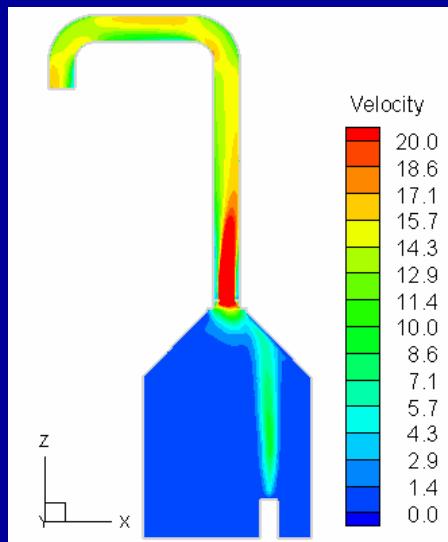
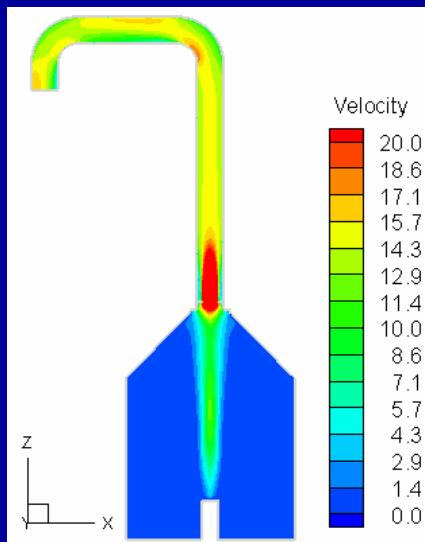
- ✓ Turbulent model : Std. k- ϵ model with buoyancy modification
- ✓ Density : Incompressible ideal gas
- ✓ Pressure-velocity coupling : SIMPLE algorithm
- ✓ Differential scheme : 2nd order upwind scheme

Fire Source Model:

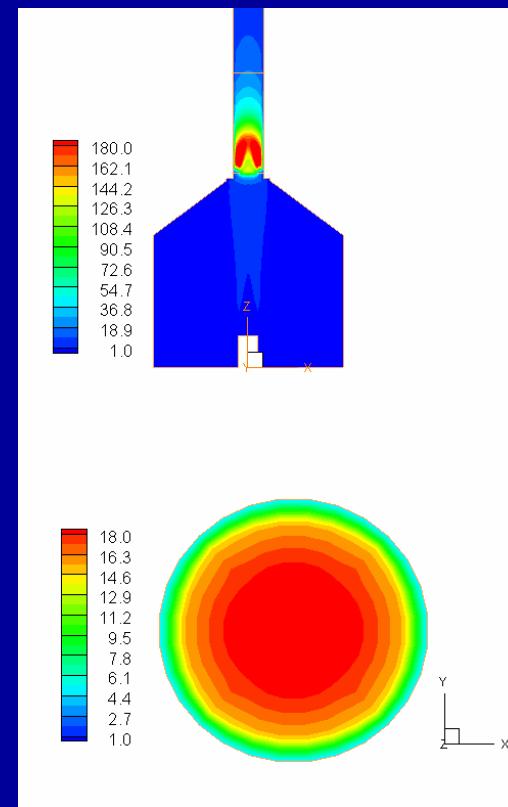
Volumetric heat and mass source model (VHMS)



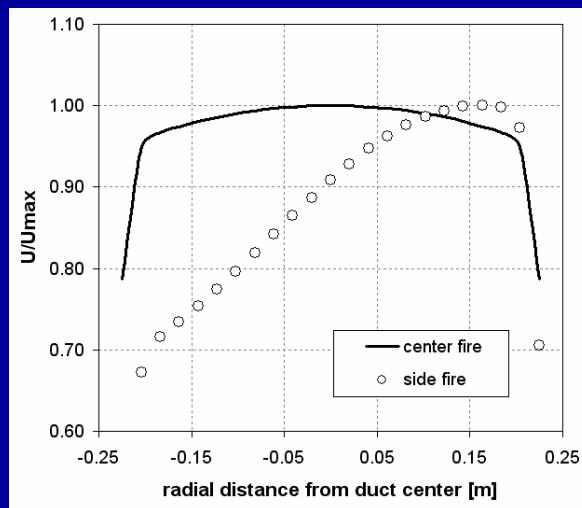
CFD modeling results 200 kW methane fire, 3 m Hood



Velocity Fields

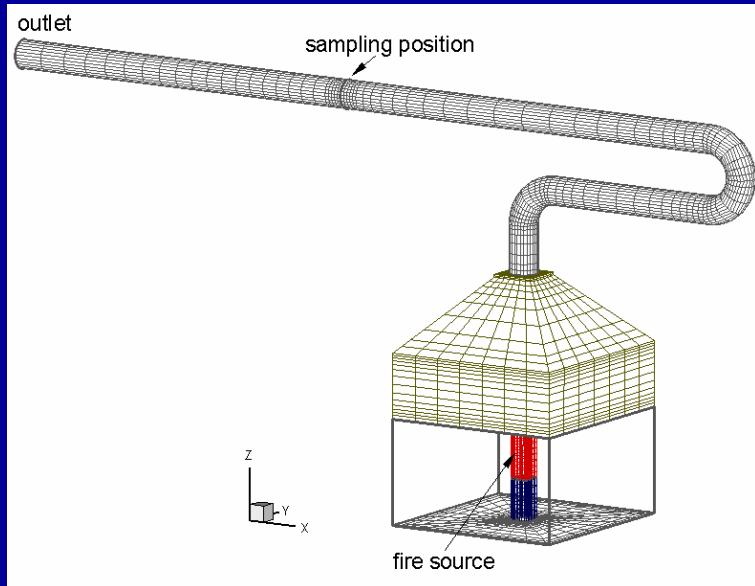


Turbulent Kinetic Energy

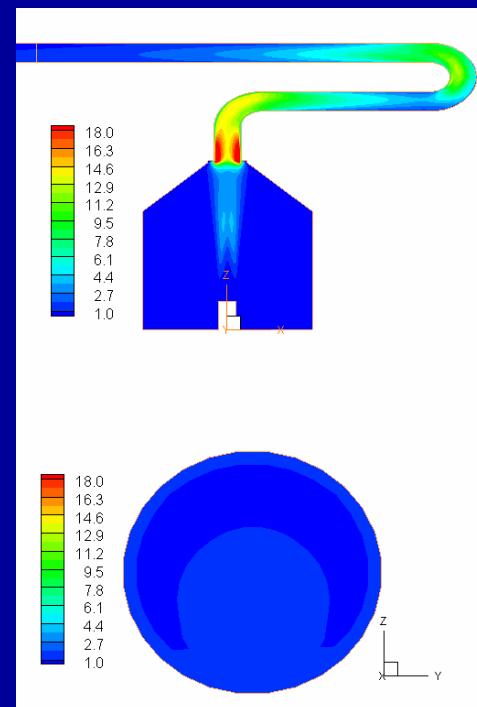


Velocity Profiles

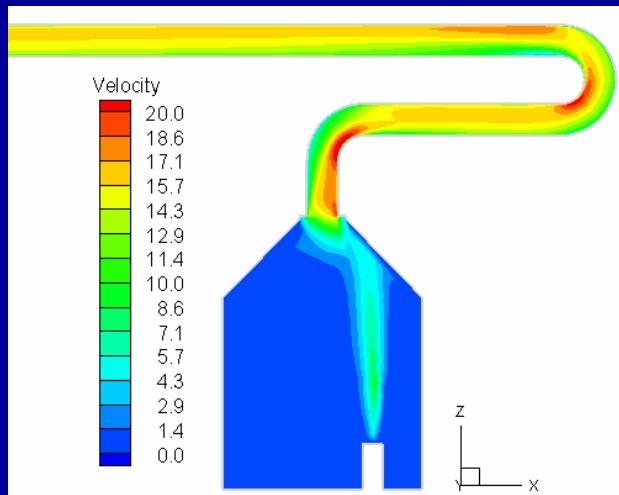
CFD modeling results



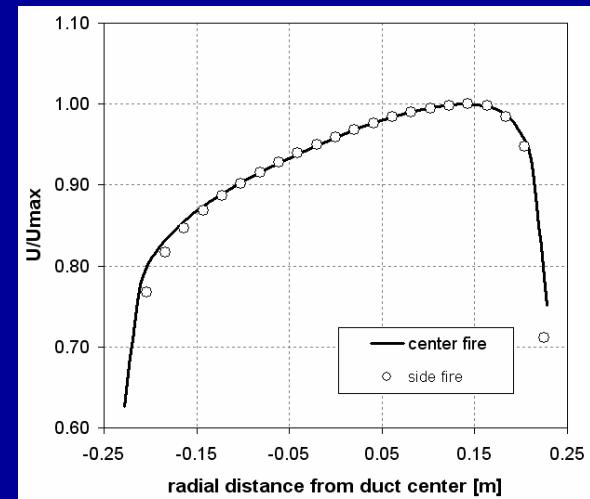
New design for exhaust duct geometry



Turbulent kinetic energy



Velocity field



Velocity profile

New Exhaust Flow Rate Measurement 500 kW Calorimeter

Reconfigured Exhaust Duct Configuration (Jan 2007)

- 50 feet of new ductwork added
- Instrumentation now on horizontal section of duct

Averaging Pitot Tube:

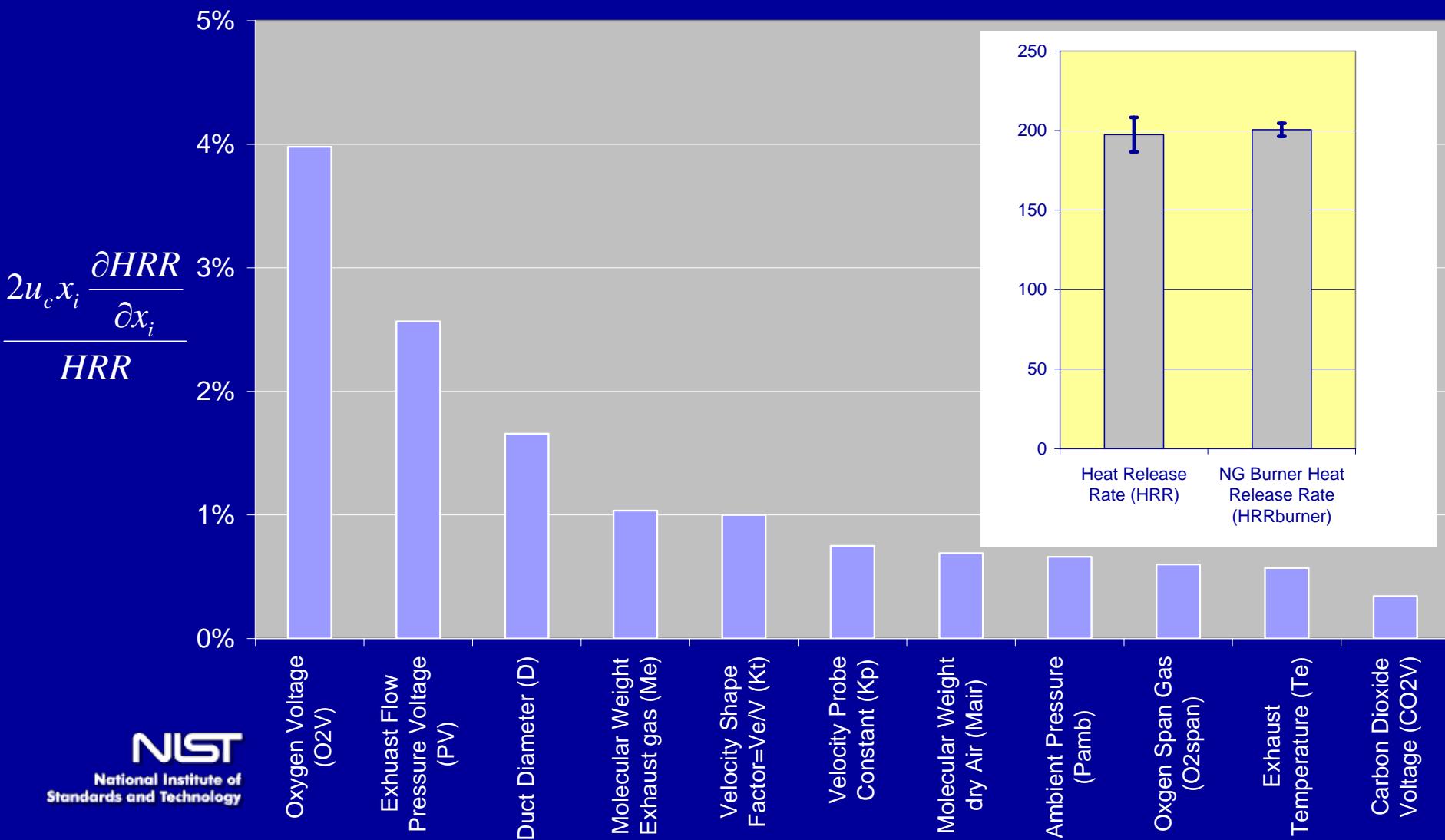
- Insensitive to small changes in velocity profile shape
- Probe constant uncertainty = 0.75 %
- Needs to be tested with highly sooting fires



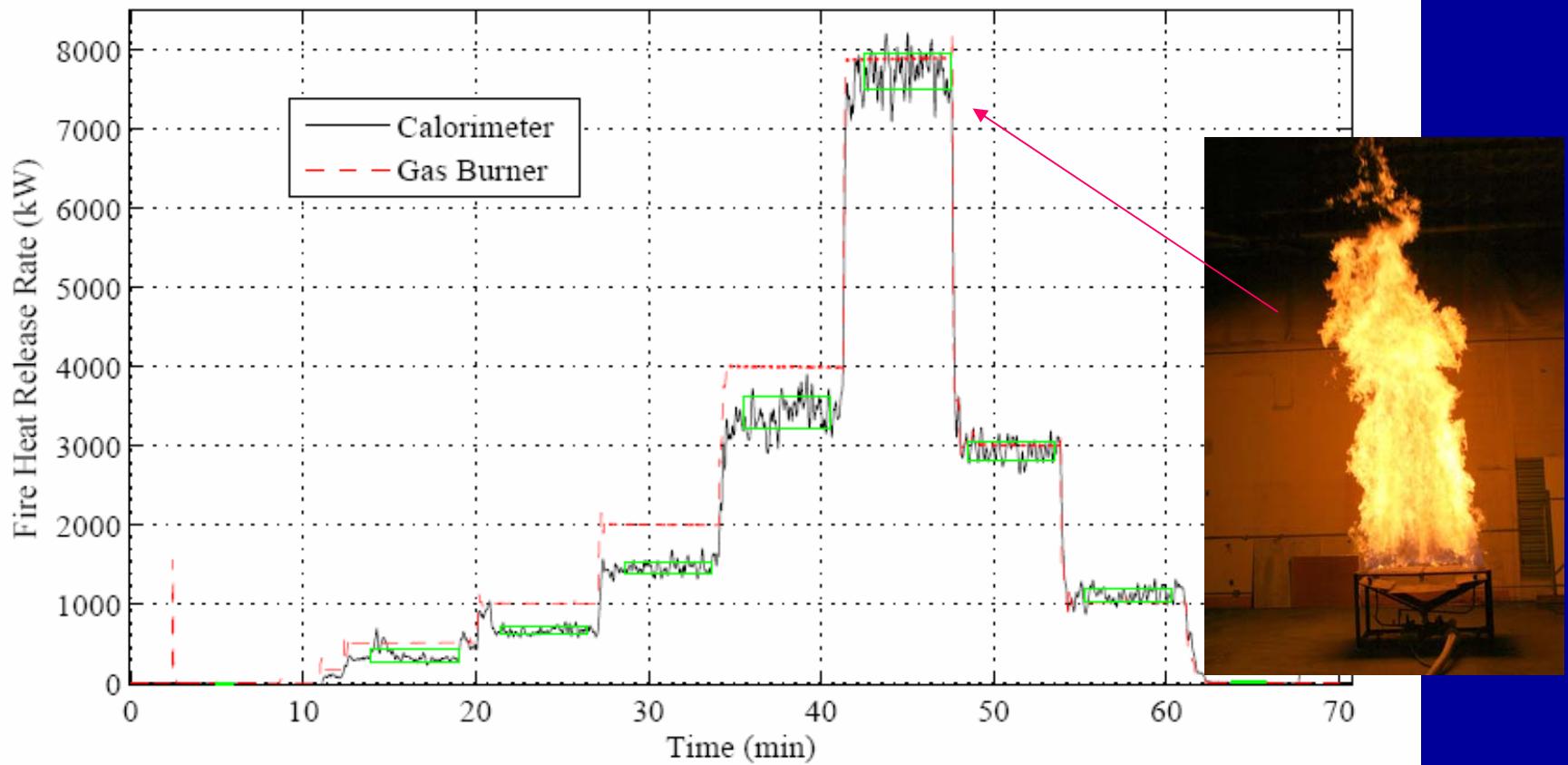
Example: Uncertainty Results – Verification

200 kW steady natural gas fire, 3 m x 3 m hood, 2 kg/s (2007 config.)

$U_{HRR} = 5.5\%$ (known fuel), $U_{HRR} = 8\%$ (unknown fuel),
 $U_{HRR} = 8\%$ (unknown fuel and fire position)

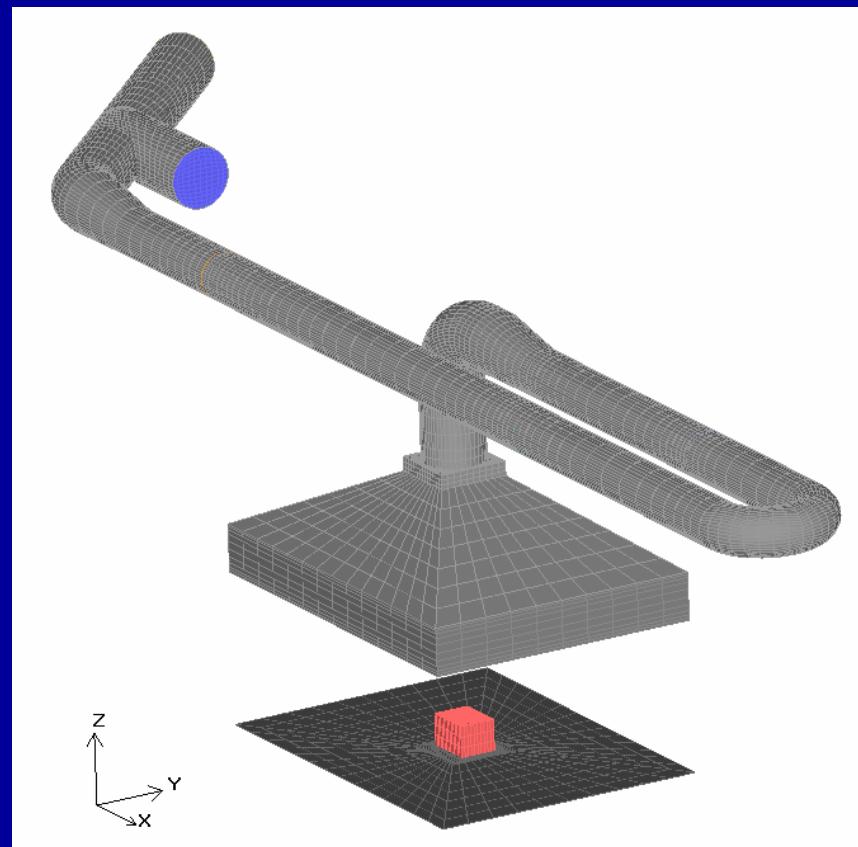
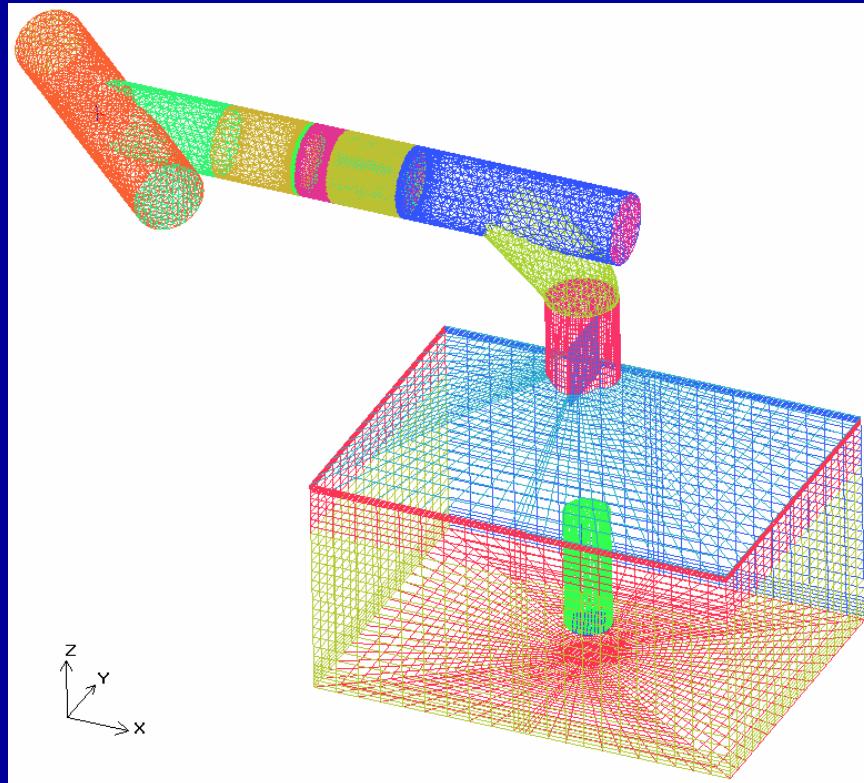


10 MW Calorimeter, Natural Gas Verification Fire Test



Future Plans

- Proposed modification to 10 MW calorimeter



Summary

- Completed new design and installation of the 500 kW calorimeter (3 m x 3 m hood) exhaust duct
- A new method for exhaust flow measurement has been implemented in the 500 kW calorimeter
- Recent changes in the 500 kW calorimeter have significantly reduced the uncertainty in the HRR measurement
- A plan for reducing the uncertainty in the 10 MW calorimeter (9 m x 12 m hood) has been developed